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# RESEARCH MEMORANDUM

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SEVERAL INTERCHANGEABLE TIP CONTROLS ON A 60° DELTA  
WING AT MACH NUMBERS OF 1.41, 1.62, AND 1.96

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NATIONAL ADVISORY COMMITTEE  
FOR AERONAUTICS

WASHINGTON  
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CONTROL HINGE-MOMENT AND EFFECTIVENESS CHARACTERISTICS OF  
SEVERAL INTERCHANGEABLE TIP CONTROLS ON A  $60^\circ$  DELTA  
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## SUMMARY

Several tip controls have been investigated on a  $60^\circ$  delta wing to supplement information previously obtained with tip controls on the same wing plan form. Effects of changes in control leading-edge sweep and trailing-edge sweep on control hinge-moment and effectiveness characteristics were determined for both fence-off and fence-on conditions. Effects of skewing the  $60^\circ$  half-delta tip-control-wing combination were also determined. The aerodynamic characteristics of the complete wing-body combination, as well as the control hinge moments and bending moments, were obtained for an angle-of-attack range of  $\pm 12^\circ$  and for control deflections up to  $20^\circ$  at Mach numbers of 1.41, 1.62, and 1.96, and Reynolds numbers of  $2.4 \times 10^6$ ,  $2.25 \times 10^6$ , and  $2.0 \times 10^6$ , respectively.

The results indicate that the nonlinear hinge-moment variations with deflection which appear to be associated with the angular gap between the wing and control forward of the hinge line were not improved by changes in control leading-edge sweepback from  $60^\circ$  to  $75^\circ$ , by changes in control trailing-edge sweep from  $-37.5^\circ$  to  $15^\circ$ , or by  $\pm 10^\circ$  skew of the control parting line and hinge line.

The balance characteristics at  $0^\circ$  control deflection and  $0^\circ$  angle of attack for the half-delta tip controls having the same hinge-line locations were essentially unchanged by variation of control leading-edge sweep angles from  $45^\circ$  to  $75^\circ$ .

The control effectiveness per unit area was little affected by increasing the control trailing-edge sweep to  $15^\circ$ , but was considerably decreased at angles of attack above zero by increasing the leading-edge sweep from  $60^\circ$  to  $75^\circ$ .

The only appreciable effects of wing skew were large negative increases in hinge moment at high angles of attack and positive control deflections when the wing panel was skewed back  $10^\circ$ .

## INTRODUCTION

The half-delta tip control has been shown in wind-tunnel and free-flight tests to be a good lateral-control device at transonic and supersonic speed (refs. 1 to 3), and with the proper hinge-line location to have relatively low hinge moments over a limited Mach number range. For closely balanced tip controls, however, nonlinear variations of hinge moment occur with both angle of attack and deflection. The investigation of reference 4 has shown that the effects of control plan form on tip control balance characteristics were secondary to the ratio of control balance area to total area. The changes in control plan form in the tests of reference 4, however, did not alter the  $60^\circ$  delta wing plan form except in one case. It is, therefore, of interest to determine the effect of changes in control leading-edge and trailing-edge sweep angles on the nonlinear hinge-moment variations and the control balance characteristics as well as on the control effectiveness characteristics. In order to furnish such information,  $45^\circ$  half-delta,  $60^\circ$  triangular, and  $75^\circ$  half-delta tip controls mounted on a  $60^\circ$  delta wing have been tested with and without fences at the control-wing juncture in the Langley 9- by 12-inch supersonic blowdown tunnel at Mach numbers of 1.41, 1.62, and 1.96, and Reynolds numbers of  $2.4 \times 10^6$ ,  $2.25 \times 10^6$ , and  $2.0 \times 10^6$ , respectively.

The aerodynamic characteristics of the complete semispan model, as well as the control hinge moments and bending moments, were obtained through an angle-of-attack range of  $\pm 12^\circ$  for control deflections up to  $20^\circ$ . Analysis of the data obtained for the  $45^\circ$  half-delta control was not made because large control torsional vibration occurred for some conditions. Data for the  $60^\circ$  half-delta control configuration of reference 1 are presented for purposes of comparison.

Also tests were made on a  $60^\circ$  half-delta control configuration with the complete wing skewed  $\pm 10^\circ$  with respect to the body axis to obtain some preliminary knowledge of the effects of wing skew on control characteristics.

## SYMBOLS

$C_L$  lift coefficient,  $\frac{\text{Lift}}{qS}$

$C_{l_{\text{gross}}}$  gross rolling-moment coefficient about wind axes,  
 $\frac{\text{Semispan wing rolling moment}}{2qSb}$

$C_{BM_F}$	control bending-moment coefficient about root chord of control surface, $\frac{\text{Bending moment}}{qS_F b_F}$
$C_h$	control hinge-moment coefficient about hinge line, $\frac{\text{Hinge moment}}{qS_F \bar{c}_F}$
$C_l, \Delta C_L$	increment in gross rolling-moment coefficient, and lift coefficient due to deflection of control surface
$q$	free-stream dynamic pressure
$S$	area of basic semispan wing with $60^\circ$ half-delta control (including area blanketed by fuselage)
$S_F$	control-surface area
$c$	local wing chord
$\bar{c}_F$	mean aerodynamic chord of control
$X_h$	distance from hinge line to control leading edge measured along $\bar{c}_F$
$b$	wing span (twice distance from rolling-moment reference axis to wing tip with $60^\circ$ half-delta control)
$b_F$	control surface span (distance from parting line to tip)
$\alpha$	angle of attack measured with respect to free-stream direction
$\delta$	control-surface deflection measured with respect to wing-chord plane
$R$	Reynolds number based on mean aerodynamic chord of wing
$M$	Mach number

## Subscripts:

$\alpha$	slope of curve of coefficient plotted against $\alpha$ ; for example, $C_{h_\alpha} = \frac{dC_h}{d\alpha}$
$\delta$	slope of curve of coefficient plotted against $\delta$ ; for example, $C_{h_\delta} = \frac{dC_h}{d\delta}$

## DESCRIPTION OF MODEL

The principal dimensions of the semispan delta wing model and the tip controls tested are shown in figure 1. A photograph of the model with the  $60^\circ$  half-delta control is shown in figure 2. The model had a leading-edge sweep of  $60^\circ$  and a corresponding aspect ratio of 2.3.

The main wing panel was made of solid steel and had modified hexagonal airfoil sections of constant thickness. The thickness ratio varied from 2.4 percent at the wing root to 9.2 percent at the wing control parting line. The wedge angles of the leading and trailing edges, measured parallel to the air stream, were  $6.78^\circ$  and  $13.80^\circ$ , respectively. The leading-edge wedge was modified by a small nose radius.

The  $45^\circ$  half delta, the two  $60^\circ$  triangular, and the  $75^\circ$  half-delta tip controls shown in figure 1(b) were tested during the present investigation. The  $60^\circ$  half-delta tip control shown in figure 1(a) was tested during the present investigation and also during the investigation reported in reference 1. The controls, which rotated about an axis in the wing perpendicular to the root chord, made up the outer portion of the wing and were separated from the inner wing panel by a streamwise parting line. The control surfaces had 3.0-percent-thick double-wedge airfoil sections and the leading edges were modified by a small nose radius. They were constructed of either solid steel or beryllium-copper. For part of the investigation a fence was mounted on the wing panel at the wing control parting line. The fence, dimensions of which are given in figure 1, was of sufficient size to seal the angular gap between the control surface and the wing panel at the highest deflection angles.

Details of the half fuselage (a body of revolution with a 0.25-inch shim), which was used in all of the tests, are also shown in figure 1.

## TUNNEL

The tests were conducted in the Langley 9- by 12-inch supersonic blowdown tunnel, which is a nonreturn tunnel utilizing the compressed air from the Langley 19-foot pressure tunnel. The inlet air enters at an absolute pressure of about  $2\frac{1}{3}$  atmospheres and contains about 0.3 percent of water by weight. The compressed air is conditioned to insure condensation-free flow in the test section by being passed through a silica gel dryer and then through banks of finned electrical heaters. Criteria for condensation-free flow were obtained from reference 5. Turbulence damping screens are located in the settling chamber. Interchangeable nozzle blocks provide three test-section Mach numbers.

Properties of the conditioned air and deviations from the average flow conditions in the test section with the tunnel clear, as determined from extensive calibration tests and reported in reference 6, are presented in the following table:

Variable	Nominal Mach number		
	1.41	1.62	1.96
Maximum deviation in Mach number . . . . .	$\pm 0.02$	$\pm 0.01$	$\pm 0.02$
Maximum deviation in ratio of static to stagnation pressure, percent . . . . .	$\pm 2.0$	$\pm 1.3$	$\pm 2.2$
Maximum deviation in stream angle, deg . .	$\pm 0.25$	$\pm 0.20$	$\pm 0.20$
Maximum dewpoint temperature, $^{\circ}\text{F}$ . . . . .	20	-5	-20
Minimum stagnation temperature, $^{\circ}\text{F}$ . . . . .	120	125	165

#### TEST TECHNIQUE

Semispan models are cantilevered from a five-component strain-gage balance mounted flush with the tunnel floor. The model rotates with the balance as the angle of attack is changed and the aerodynamic forces and moments on the wing-fuselage combination are measured with respect to the body axis and then rotated to the wind axis to determine the coefficients presented. For the skewed wing tests, the  $60^{\circ}$  delta wing was skewed  $\pm 10^{\circ}$  from its original attitude with respect to the half body. The aerodynamic forces and moments were measured with respect to the same body axis, but in computing the data, the reference axes were rotated  $10^{\circ}$  to simulate the skewed positions. Angle-of-attack loading and body effects would not correctly simulate those of a wing in a yawed attitude, but for an outboard control at supersonic speeds, loading due to control  $\delta$  should be approximately the same as if the complete model were yawed. In order to minimize the tunnel-wall boundary-layer effects on the flow over the cylindrical fuselage, models are shimmed out from the tunnel floor 0.25 inch (ref. 7). Because of balance deflection under load, a clearance gap of 0.010 to 0.020 inch is maintained between the fuselage shim and the tunnel floor.

The hinge moments and bending moments on the tip controls were measured by means of an optical system which was developed for use with wings too thin to permit conventional strain-gage installation.

The optical system consists primarily of two high intensity light sources mounted upon a large circular plexiglass screen with a radius of 80 inches, and two mirrors adjacent to each other (0.070 inch in diameter) installed flush in the model control surfaces and wing panel.

Reflection of the two light images upon the screen show the relative displacement of the tip light image with respect to the wing light image from which the hinge moments and bending moments may be determined. For a complete description of the optical system, see reference 1.

#### ACCURACY OF DATA

An estimate of the probable errors in the present data caused by the fluctuations in the readings of the measuring equipment, instrument reading errors, and calibration errors are presented in the following table:

Variable	Control plan form		
	60° half delta	60° triangular	75° half delta
	Error	Error	Error
$\alpha$	$\pm 0.05^\circ$	$\pm 0.05^\circ$	$\pm 0.05^\circ$
$\delta$	$\pm 0.2^\circ$	$\pm 0.2^\circ$	$\pm 0.2^\circ$
$C_L$	$\pm 0.0015$	$\pm 0.0015$	$\pm 0.0015$
$C_L$	$\pm 0.010$	$\pm 0.010$	$\pm 0.010$
$C_h$	$\pm 0.010$	$\pm 0.011$	$\pm 0.006$
$C_{BM_F}$	$\pm 0.020$	$\pm 0.022$	$\pm 0.018$

Because of the inaccuracies in the measurements by the optical system, the present control hinge-moment and bending-moment data do not warrant exact quantitative evaluation of the results. These inaccuracies are attributed to errors in manual control calibrations, dissimilar distortion of controls under actual aerodynamic loads and under calibrated loads, and errors arising from certain relations in the optics of the measuring system. A discussion of the latter error is given in reference 1. However on the basis of the repeated data, it appears that the estimates of the probable errors in  $C_{BM_F}$  and  $C_h$  given in the preceding table are reasonable.

#### RESULTS AND DISCUSSION

Figure 3 presents the basic aerodynamic coefficients at a Mach number of 1.96 plotted against angle of attack for the wing-fuselage combination with the control having 15° trailing-edge sweepback  $\left(\frac{x_h}{\bar{c}_f} = 0.413\right)$ .

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This control will hereafter be referred to as a 60° triangular control. These data are representative of the data for the other Mach numbers and tip controls which have been presented only in the form of cross plots in figures 4 to 15.

It will be noted in figure 3 that data were obtained for positive control deflections at both negative and positive angles of attack. Such data were used to obtain data for negative control deflections at positive angles of attack by reversing the signs of the angles and coefficients. This method of handling the data was possible because the model had symmetrical airfoil sections.

#### Effects of Plan Form With Fence Off

Hinge moments. - The variations of the hinge-moment coefficients with control deflections for the basic 60° half-delta control of reference 1, the 60° triangular control, and the 75° half-delta control are presented in figure 4 for angles of attack of 0° to 12°. At zero angle of attack the variation of hinge-moment coefficients with deflection tended to be fairly linear for the three control plan forms. Hinge-moment coefficients due to deflection at zero angle of attack were slightly underbalanced for the 60° and 75° half-delta controls with  $\frac{X_h}{\bar{c}_f} = 0.455$ , but the amount of underbalance for the 60° triangular control with  $\frac{X_h}{\bar{c}_f} = 0.413$  was considerably greater.

As the angles of attack were increased, the variation of hinge-moment coefficients with control deflection became increasingly nonlinear for all three controls. The nonlinearities were such that the values of  $C_{h\delta}$  which were zero or negative at positive deflections became positive for the 60° and the 75° half-delta controls as the control deflection decreased through zero. Values of  $C_{h\delta}$  for the less closely balanced 60° triangular control generally increased positively as the control deflection decreased through zero but became positive only at 8° angle of attack for  $M = 1.41$  and 12° angle of attack for  $M = 1.62$ . Data from tests of a similar wing-control configuration at  $M = 1.61$  (ref. 4) showed similar hinge-moment nonlinearities existed when the control trailing edge was swept forward from 0° to -37.5°.

It is thus shown that the positive increases in  $C_{h\delta}$  which occurred for the basic 60° half-delta control at moderate angles of attack as the control deflection was decreased near zero were not eliminated by increasing the control leading-edge sweep to 75°, by increasing the

control trailing-edge sweep to  $15^\circ$ , or by decreasing the control trailing-edge sweep to  $-37.5^\circ$ . Reference 1 showed that these nonlinearities were apparently typical of controls having tip balance areas extending from the hinge line to the wing leading edge. Consequently, it appears that these nonlinearities are associated with the angular gap between the wing and control as the control unports.

Static hinge-moment and effectiveness data are not presented for the  $45^\circ$  half-delta control because of large torsional control vibration which occurred at angles of attack when the angle of attack was approximately equal to the control deflection but of opposite sign. Figure 5 was prepared to illustrate the angles of attack and deflections for which the vibrations occurred. In order to give some indication of the magnitude of the vibrations, three degrees of intensity were used, the rough index being the plus and minus change in indicated hinge moment from a neutral value. As the Mach number increased, the vibrations became less severe and within the range of conditions for which the vibration occurred, the intensity of the vibrations increased as the angle of attack decreased and as the deflection increased.

Values of the slope parameters  $C_{h_\alpha}$  and  $C_{h_\delta}$  for the  $45^\circ$  half-delta control, being unaffected by vibration at small angles of attack or small deflections, are presented in table I together with those for the  $60^\circ$  and  $75^\circ$  half-delta control. At all Mach numbers only small differences in  $C_{h_\alpha}$  and  $C_{h_\delta}$  were evidenced for these controls, which had

identical hinge-line locations  $\left(\frac{x_h}{c_f} \approx 0.455\right)$ , although the control

leading-edge sweep angle varied from  $45^\circ$  to  $75^\circ$ . Reasonable agreement with the experimental correlation of reference 4 (based on the ratio of balance area to total area for several tip controls) was also shown at  $M = 1.62$  (see table I).

Control bending moments.— Bending-moment coefficients for the  $60^\circ$  triangular, and the  $60^\circ$  and  $75^\circ$  half-delta controls are presented in figure 6 cross plotted against deflection. In general, systematic variations of  $C_{BM_f}$  with angle of attack and deflection were noted for the three controls. For the  $60^\circ$  and  $75^\circ$  half-delta controls, the  $C_{BM_f}$  curves were more linear than those for the  $60^\circ$  triangular control. The magnitudes of  $C_{BM_f}$  for the  $60^\circ$  triangular and the  $60^\circ$  half-delta controls were about equal, and the magnitudes for the  $75^\circ$  half-delta control were about one third smaller than for the other two controls.

Rolling moment.— For zero angle of attack, rolling-moment coefficients increased with increasing deflection for the three plan forms (fig. 7). The rate of increase with deflection  $C_{l_\delta}$  did not vary

appreciably with  $\delta$  for the  $60^\circ$  triangular and  $60^\circ$  half-delta controls for zero angle of attack, but decreased considerably with increasing deflection for the  $75^\circ$  half-delta control at  $M = 1.41$ . Increasing the angle of attack or increasing the deflection at angles of attack above zero tended to decrease the parameter  $C_{l\delta}$  for positive deflection.

For the  $60^\circ$  triangular and the  $75^\circ$  half-delta controls at  $M = 1.41$ , the decrease in  $C_{l\delta}$  became progressively more pronounced until a value of deflection was reached (at  $\alpha = 12^\circ$ ) beyond which further increases in deflection caused decreases in rolling moment. For the  $60^\circ$  half-delta control, similar results were shown in reference 1 for higher angles of attack. In the negative deflection range the changes in  $C_{l\delta}$  with angle of attack were considerably less pronounced than at positive deflections, and were somewhat erratic. In general, the roll effectiveness  $C_{l\delta}$  of the  $60^\circ$  half-delta control and the  $60^\circ$  triangular control were approximately equal, although the area of the  $60^\circ$  half-delta control was slightly smaller. The roll effectiveness for the  $75^\circ$  control was considerably less than for the other two controls, which was to be expected because of its smaller area. Rolling moment per unit area was, however, more nearly equal for all three controls at zero angle of attack - the  $60^\circ$  half-delta control having the highest effectiveness and the  $75^\circ$  half-delta the lowest. As the angle of attack was increased though, the loss in effectiveness per unit area for the  $75^\circ$  half-delta control was considerably greater than for the other two controls.

Incremental lift effectiveness. - The trends of the  $\Delta C_L$  variations with angle of attack and deflection (fig. 8) were similar to those shown by the rolling-moment data. That is,  $\Delta C_{L\delta}$  at positive deflections decreases with increases in angle of attack and deflection, and effects at negative deflections were much less pronounced.

Also values of  $\Delta C_L$  were much less for the  $75^\circ$  half-delta control than for the other two controls, and were in general, about equal for the  $60^\circ$  half-delta and the  $60^\circ$  triangular controls.

#### Effects of Plan Form With Fence On

Data obtained with a fence installed at the wing control parting line are presented in figures 9 to 12 together with the fence-off data. It should be noted that the  $60^\circ$  triangular control used for the fence-on tests was slightly smaller and had a more rearward hinge-line location (see fig. 1) than the  $60^\circ$  triangular control used for fence-off tests. For this reason, the fence-on and fence-off data for these controls can be compared directly only insofar as trends are concerned.

In general, the data showed that addition of the fences caused no major change in the effects of plan form.

The hinge-moment data of figure 9 support the conclusions of references 1, 8, and 9 in that addition of the fence at the control parting line reduced the nonlinear variations of hinge moment with both angle of attack and deflection. It appears likely that the nonlinearities in the hinge-moment variation with deflection which occur at moderate to large angles of attack near zero deflection would have been reduced by use of a partial-chord fence extending only from the wing leading edge to the control hinge line. Data of references 8 and 9 show that similar nonlinear hinge-moment variations with deflection were successfully eliminated or delayed to higher angles of attack and more negative deflections by use of the partial chord fence on a horn-balanced flap-type control and a  $60^\circ$  half-delta control. These data indicate that these nonlinearities are associated principally with the gap between wing and tip balance area forward of the hinge line rather than with the plan form of the control.

The addition of the fence had only minor effects on the variation with deflection of  $C_{BM}$ ,  $C_L$  and  $\Delta C_L$  as shown by figures 10, 11, and 12, respectively.

#### Effects of Skewing Wing

Hinge moments.- Data of figure 13 show that, at low angles of attack, the shape of the curves for  $C_h$  against  $\delta$  was changed considerably by  $\pm 10^\circ$  wing skew, but that the magnitudes were not affected to any great extent. At higher angles of attack, however, skewing the wing forward at  $M = 1.41$  caused increases in  $C_h$  at negative deflections, and skewing the wing backward at  $M = 1.96$  caused large negative increases in  $C_h$  at positive deflections. Since the nonlinear characteristics of tip controls are not improved by changing either control leading-edge or trailing-edge sweep or by skewing the wing-control combination, it may be reasoned that no improvement would result if wing plan form were left unskewed while hinge line and parting line were skewed.

Bending moments.- In general, the data of figure 14 show that the slope of the curves for  $C_{BM_F}$  against deflection increases as the wing is skewed forward and decrease as the wing is skewed back. The data also show that the magnitudes of  $C_{BM_F}$  due to angle of attack at zero deflection increase as the wing is skewed forward and decrease as the wing is skewed back. The result is that maximum bending-moment coefficients are obtained at positive angles of attack and deflections for the wing in a skewed forward attitude.

Rolling moment. - The rolling-moment characteristics for zero angle of attack (fig. 15) indicate small increases in effectiveness with the wing skewed forward. At the higher angles of attack, the effect of skewing the wing forward was to cause a greater increase in effectiveness at negative deflections and a decrease in effectiveness at positive deflections. Skewing the wing back caused small decreases in effectiveness for all angles of attack at  $M = 1.96$ .

In considering the over-all roll effectiveness for a complete wing configuration with equal up and down deflection of opposite ailerons, the data at  $M = 1.96$  indicate that the total roll effectiveness would be little affected by  $\pm 10^\circ$  skew for zero angle of attack. However, at higher angles of attack, the roll effectiveness would be decreased if the down aileron was on the leading wing panel and would be increased if the down aileron was on the trailing wing panel.

#### CONCLUDING REMARKS

An investigation of tip controls on a  $60^\circ$  delta wing conducted in the 9- by 12-inch supersonic blowdown tunnel at Mach numbers of 1.41, 1.62, and 1.96 and supplemented by data from previous investigations indicated the following results:

1. The nonlinear hinge-moment variations with deflections characterized by a positive increase in the slope parameter  $C_{h\delta}$  at moderate angles of attack as the deflection is decreased through zero are not improved when:

- (a) the control leading edge is sweptback  $75^\circ$
- (b) the control trailing edge is sweptback  $15^\circ$
- (c) the control trailing edge is sweptforward  $37.5^\circ$
- (d) the control parting line and hinge line is skewed either  $10^\circ$  backwards or  $10^\circ$  forward.

These nonlinear variations are apparently associated principally with the gap between the wing and control forward of the hinge line since sealing the gap by a fence generally eliminates the nonlinearities.

2. The control effectiveness per unit area was little affected by increasing the control trailing-edge sweep to  $15^\circ$ , but was considerably decreased at angles of attack above zero by increasing the leading-edge sweep from  $60^\circ$  to  $75^\circ$ .

3. Values of the slope parameters  $C_{h\alpha}$  and  $C_{h\delta}$  at zero angle of attack and zero control deflection for the half-delta tip controls having hinge-line locations at 45.5 percent mean aerodynamic chord of control were essentially unchanged by variations of control leading-edge sweep from  $45^\circ$  to  $75^\circ$ .

4. Large torsional vibration occurred for the  $45^\circ$  half-delta control when the control deflection was approximately equal to the angle of attack but of opposite sign.

5. The skewed wing tests of a  $60^\circ$  half-delta control indicated that the only major effect of  $\pm 10^\circ$  wing skew were large negative increases in hinge-moment coefficients at positive control deflections and high angles of attack for the skewed back condition.

Langley Aeronautical Laboratory,  
National Advisory Committee for Aeronautics,  
Langley Field, Va., September 24, 1953.

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TABLE I

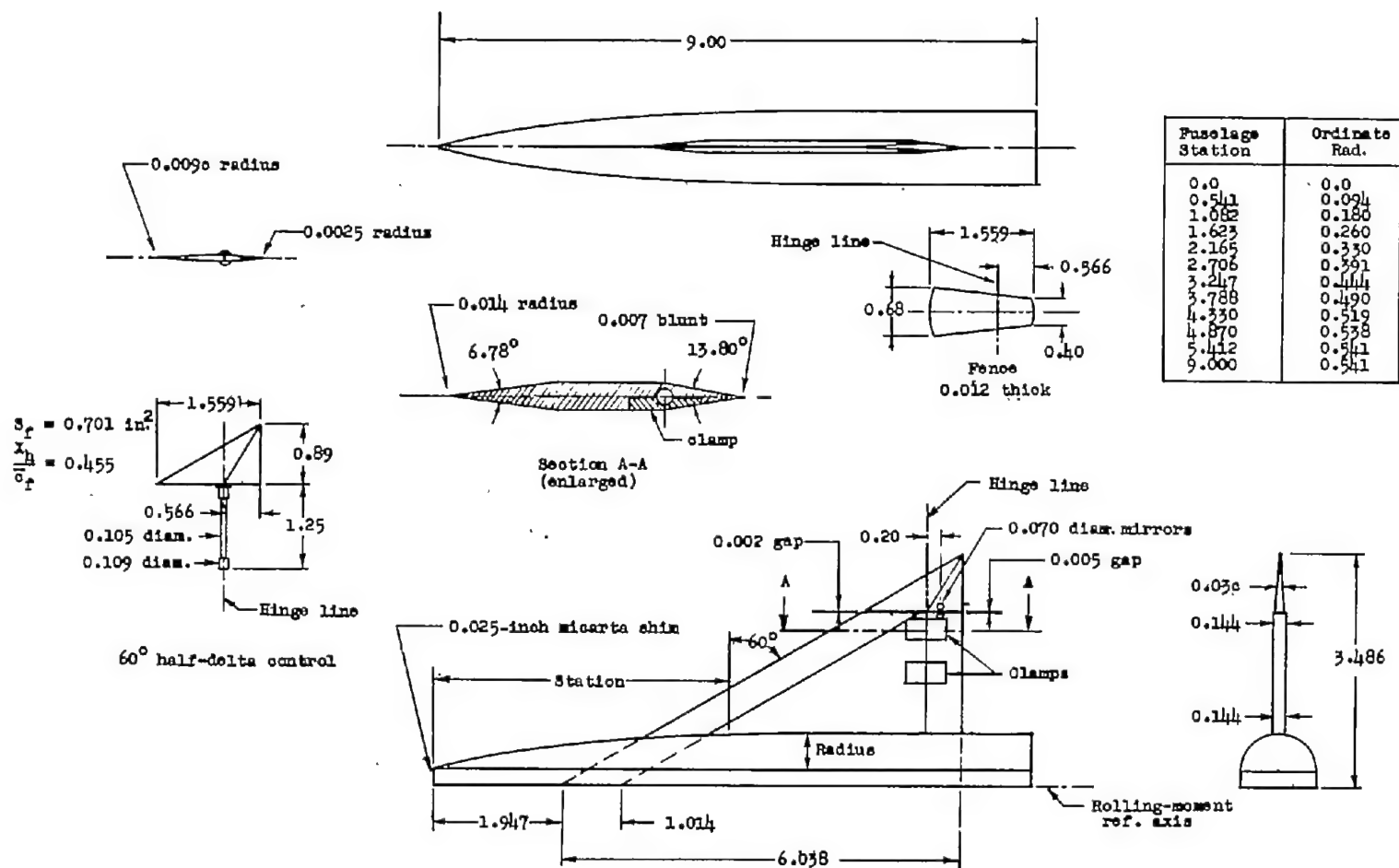
VALUES OF THE SLOPE PARAMETERS  $C_{h\alpha}$  AND  $C_{h\delta}$  AT ZERO ANGLE

OF ATTACK AND DEFLECTION FOR HALF-DELTA TIP CONTROLS

HAVING HINGE-LINE LOCATIONS AT  $\frac{x_h}{\bar{c}_f} = 0.455$ 

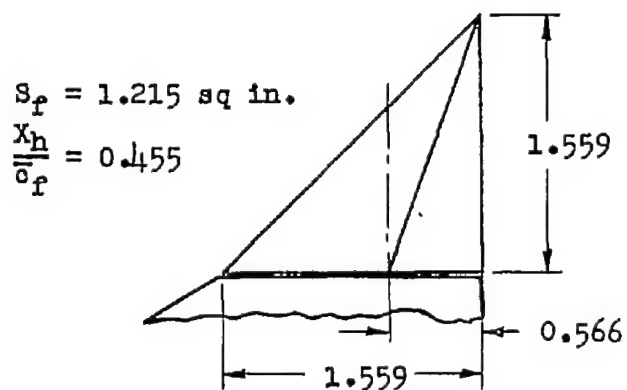
Control leading- edge sweep, (deg)	M = 1.41		M = 1.62		M = 1.96	
	$C_{h\alpha}$	$C_{h\delta}$	$C_{h\alpha}$	$C_{h\delta}$	$C_{h\alpha}$	$C_{h\delta}$
45	0.0015	-0.0015	0.00170	0	0.00170	-----
60	.00250	-.0011	.00310	-0.0010	.00320	-0.0011
75	.00120	-.0005	.00125	0	.00450	-.00075
Experimental correlation of reference 4	-----	-----	.0030	.0008	-----	-----



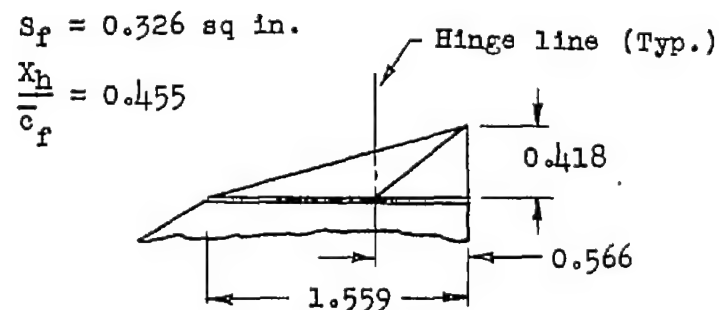


(a) Basic model showing 60° half-delta control.

Figure 1.- Details of semispan-wing-fuselage combination. Aspect ratio, 2.3; mean aerodynamic chord, 4.025 inches; half wing area, 10.524 square inches. All dimensions are in inches.

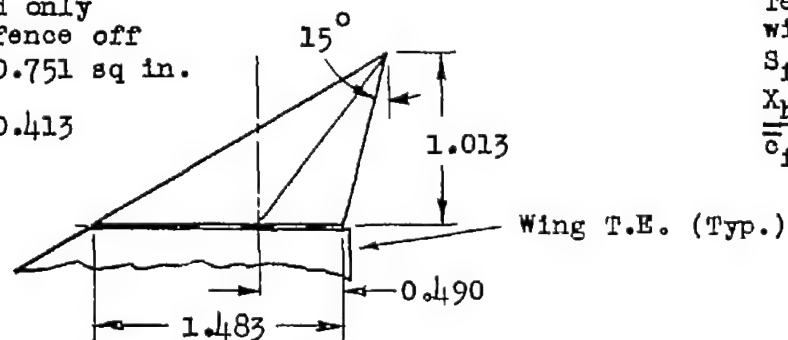


45° half-delta



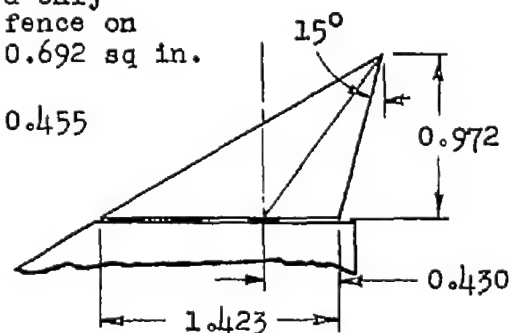
75° half-delta

Tested only  
 with fence off  
 $S_f = 0.751 \text{ sq in.}$   
 $\frac{x_h}{c_f} = 0.413$



60° triangular

Tested only  
 with fence on  
 $S_f = 0.692 \text{ sq in.}$   
 $\frac{x_h}{c_f} = 0.455$



(b) Details of tip controls. All dimensions are in inches.

Figure 1.- Concluded.

3B

NACA RM 153708a

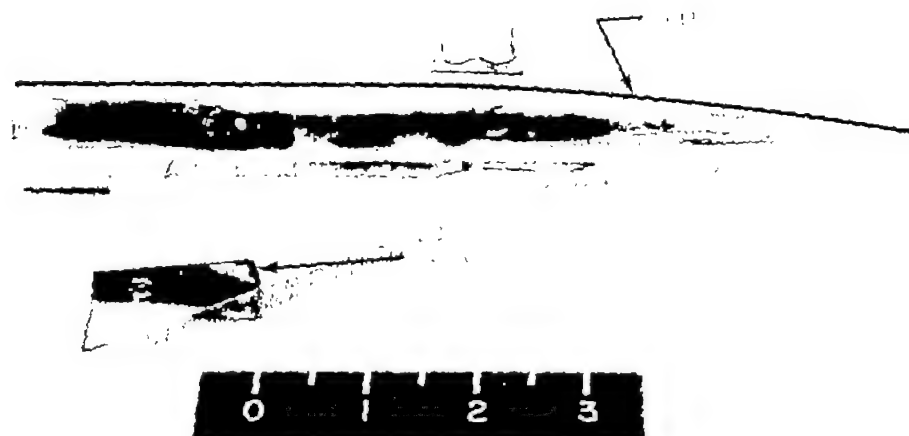
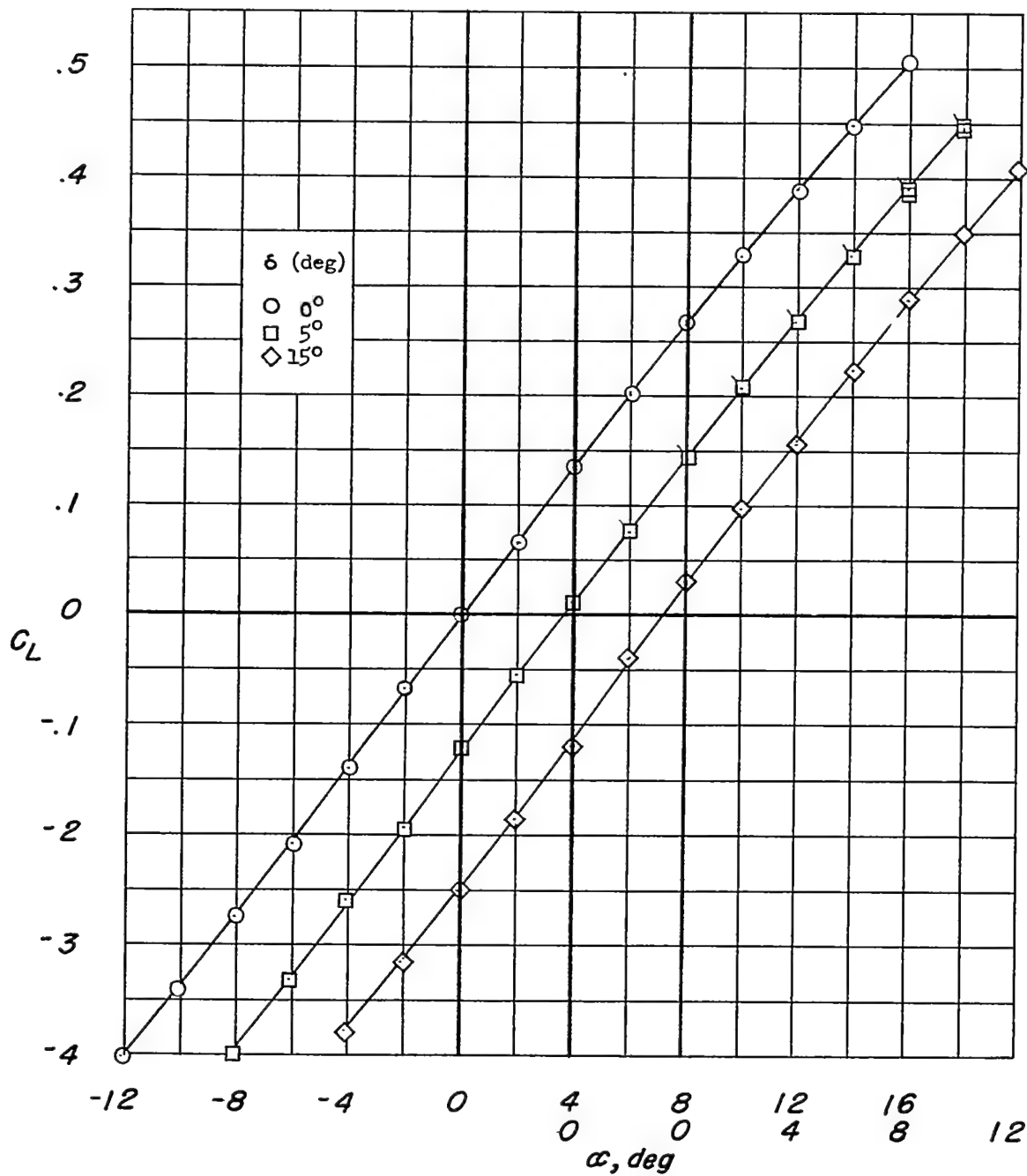


Figure 2.- Photograph of test model.

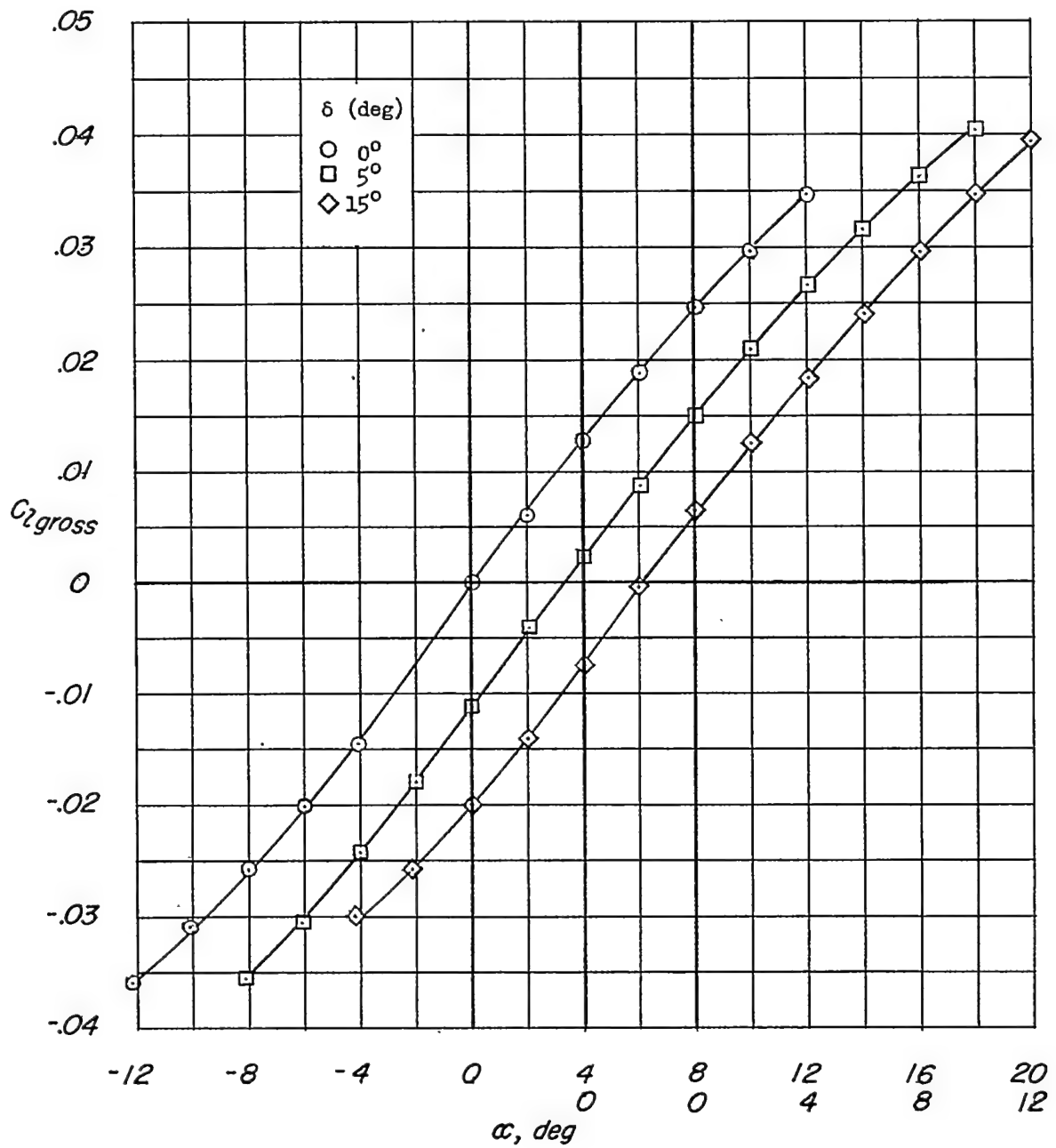
L-74730.1

17



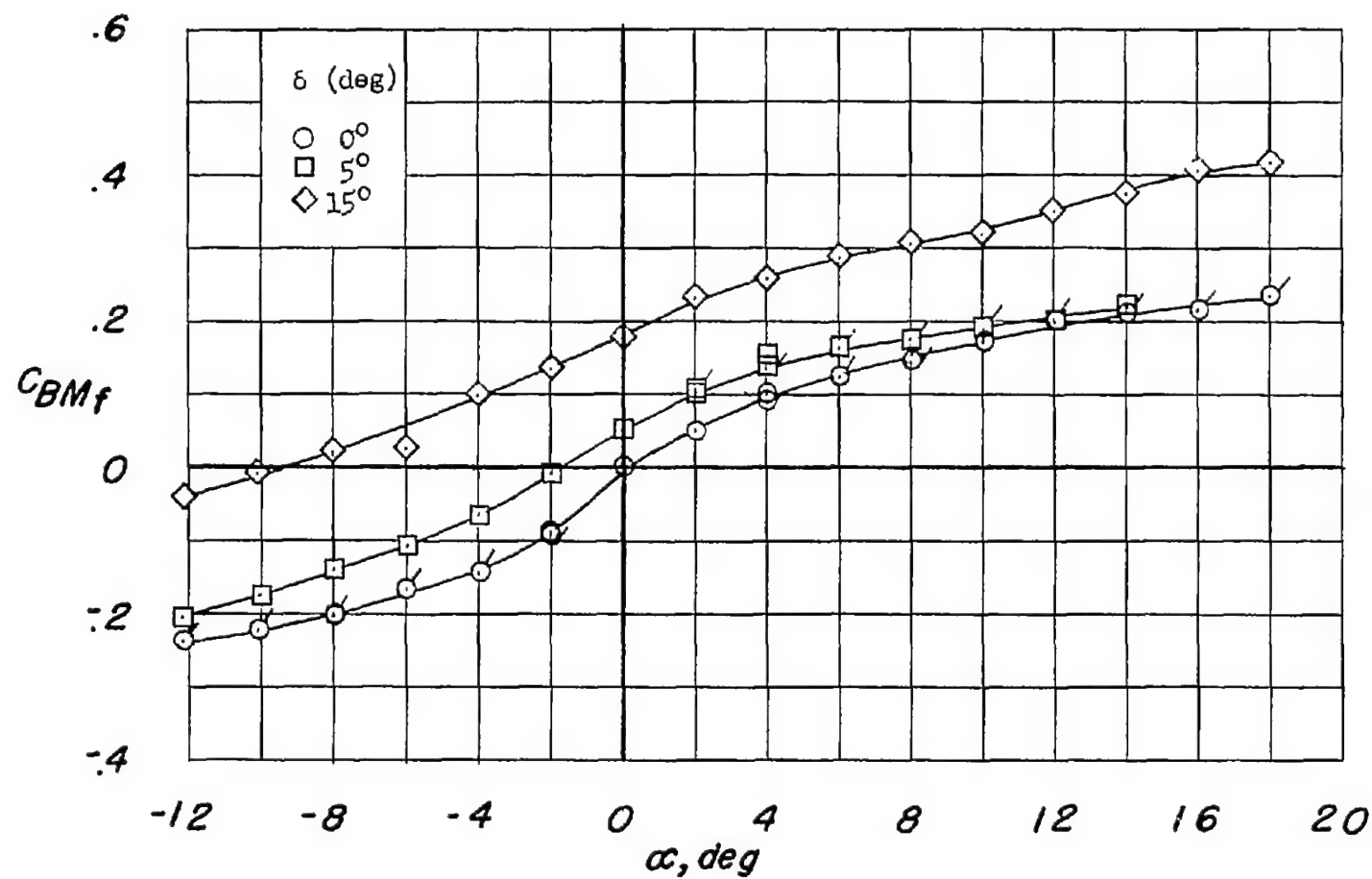
(a)  $C_L$  plotted against  $\alpha$ .

Figure 3.- Aerodynamic characteristics of a 60° triangular control on a semispan delta-wing-fuselage combination.  $\frac{x_h}{c_f} = 0.413$ ;  $R = 2.0 \times 10^6$ ;  $M = 1.96$ ; flagged symbols denote repeat tests.



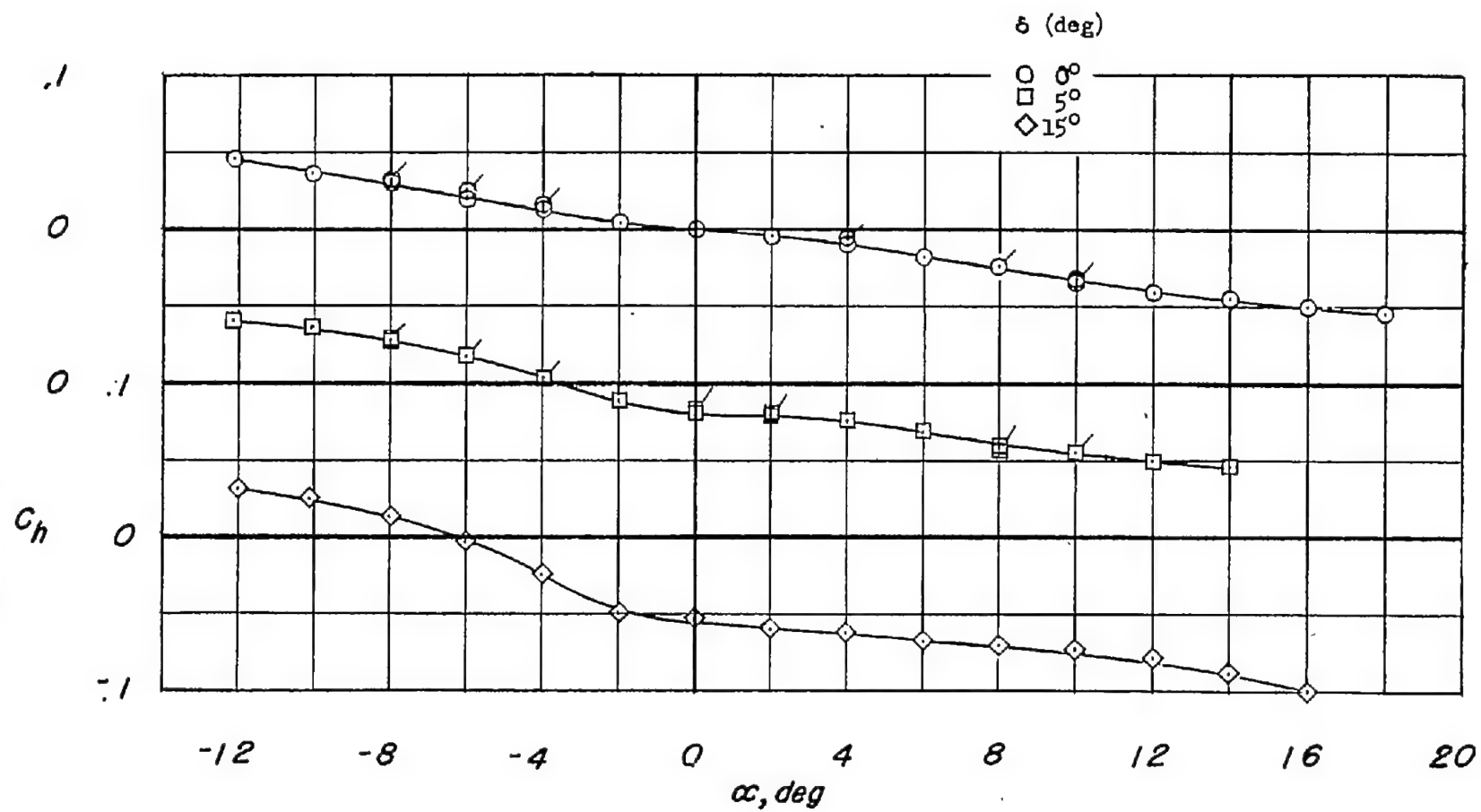
(b)  $C_{l_{gross}}$  plotted against  $\alpha$ .

Figure 3.- Continued.



(c)  $C_{BM_f}$  plotted against  $\alpha$ .

Figure 3.- Continued.



(d)  $C_h$  plotted against  $\alpha$ .

Figure 3.- Concluded.

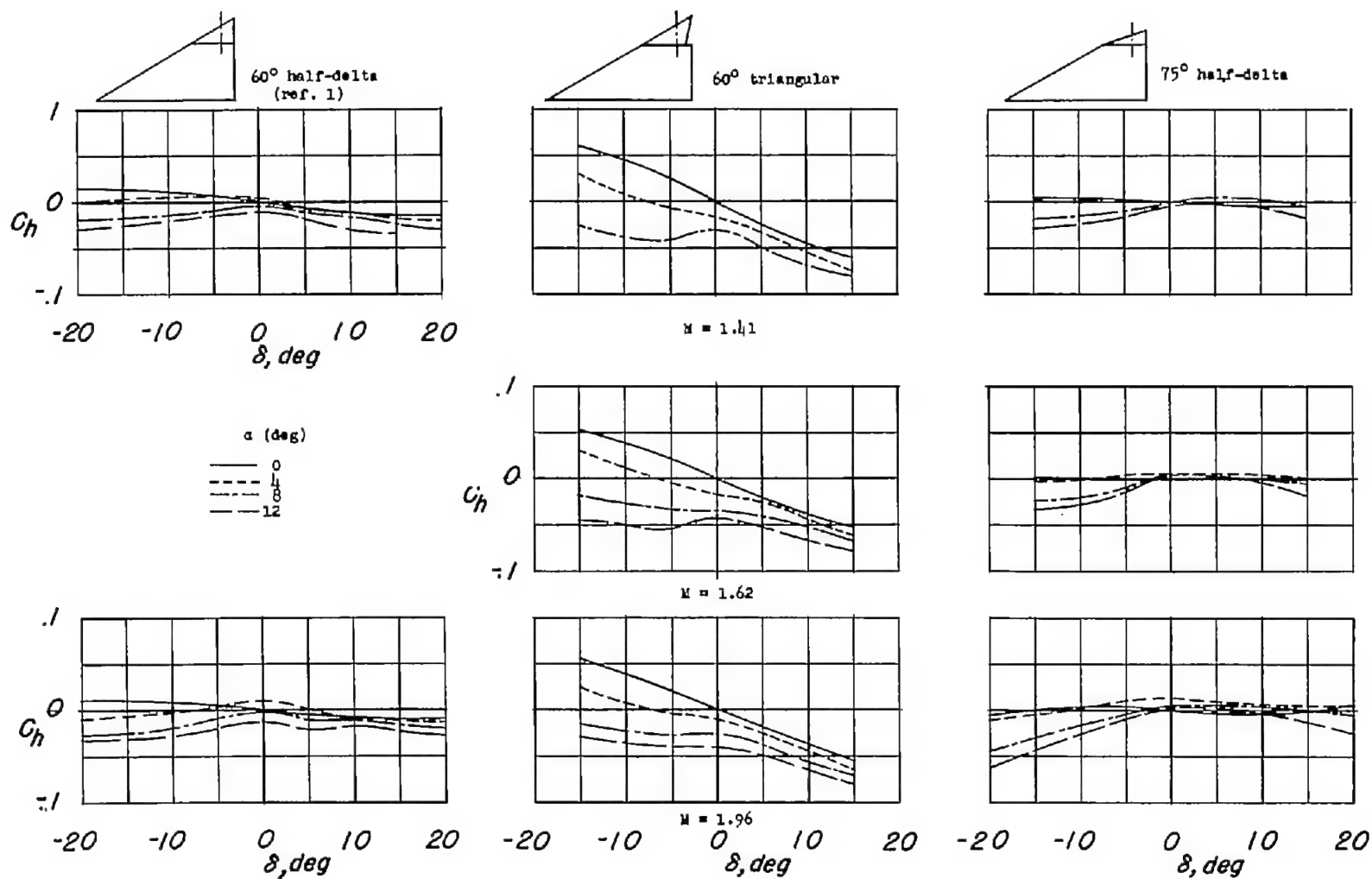
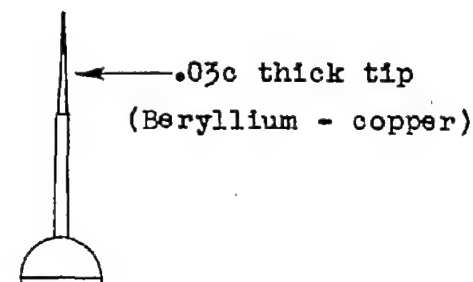
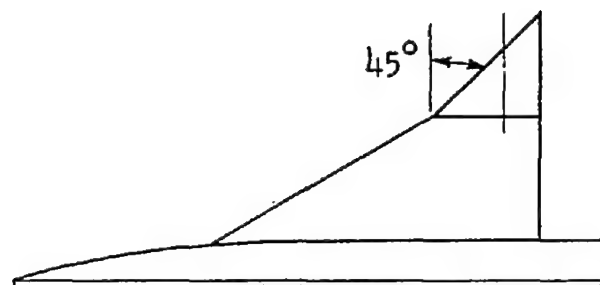





Figure 4.- Variation of hinge-moment coefficients with deflection for tip controls of three plan forms.  $R = 2.4 \times 10^6$ ,  $2.25 \times 10^6$ , and  $2.0 \times 10^6$ ;  $M = 1.41$ ,  $1.62$ , and  $1.96$ , respectively.





# Vibration

-  Slight  $\Delta C_h < \pm .02$
-  Moderate  $\Delta C_h \approx \pm .06$
-  Severe  $\Delta C_h > \pm .15$

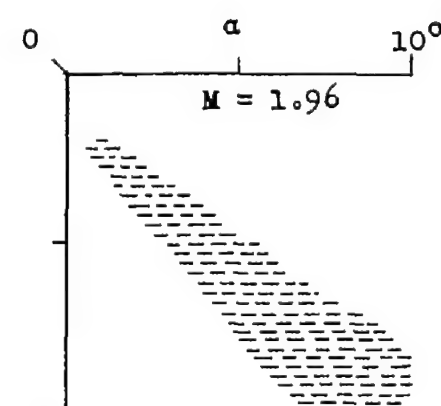
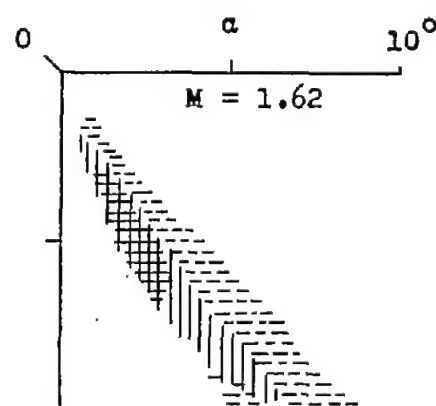
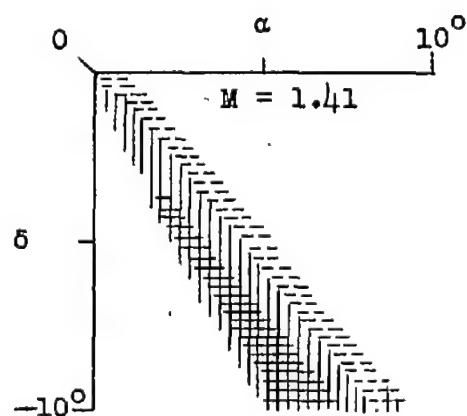


Figure 5.- Vibration of 45° half-delta tip control.

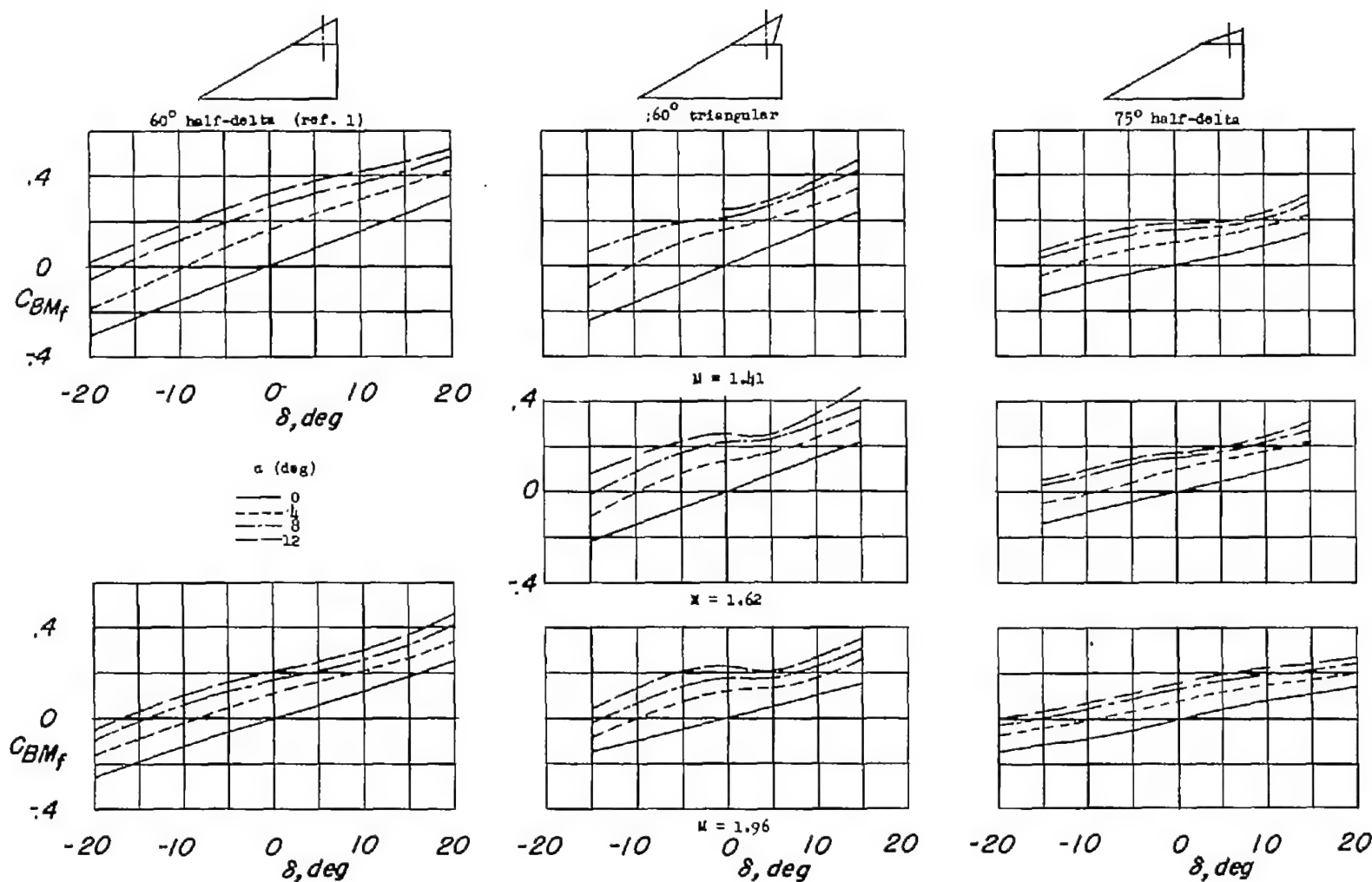


Figure 6.- Variation of bending-moment coefficient with deflection for tip controls of three plan forms.  $R = 2.4 \times 10^6$ ,  $2.25 \times 10^6$ , and  $2.0 \times 10^6$ ;  $M = 1.41$ ,  $1.62$ , and  $1.96$ , respectively.

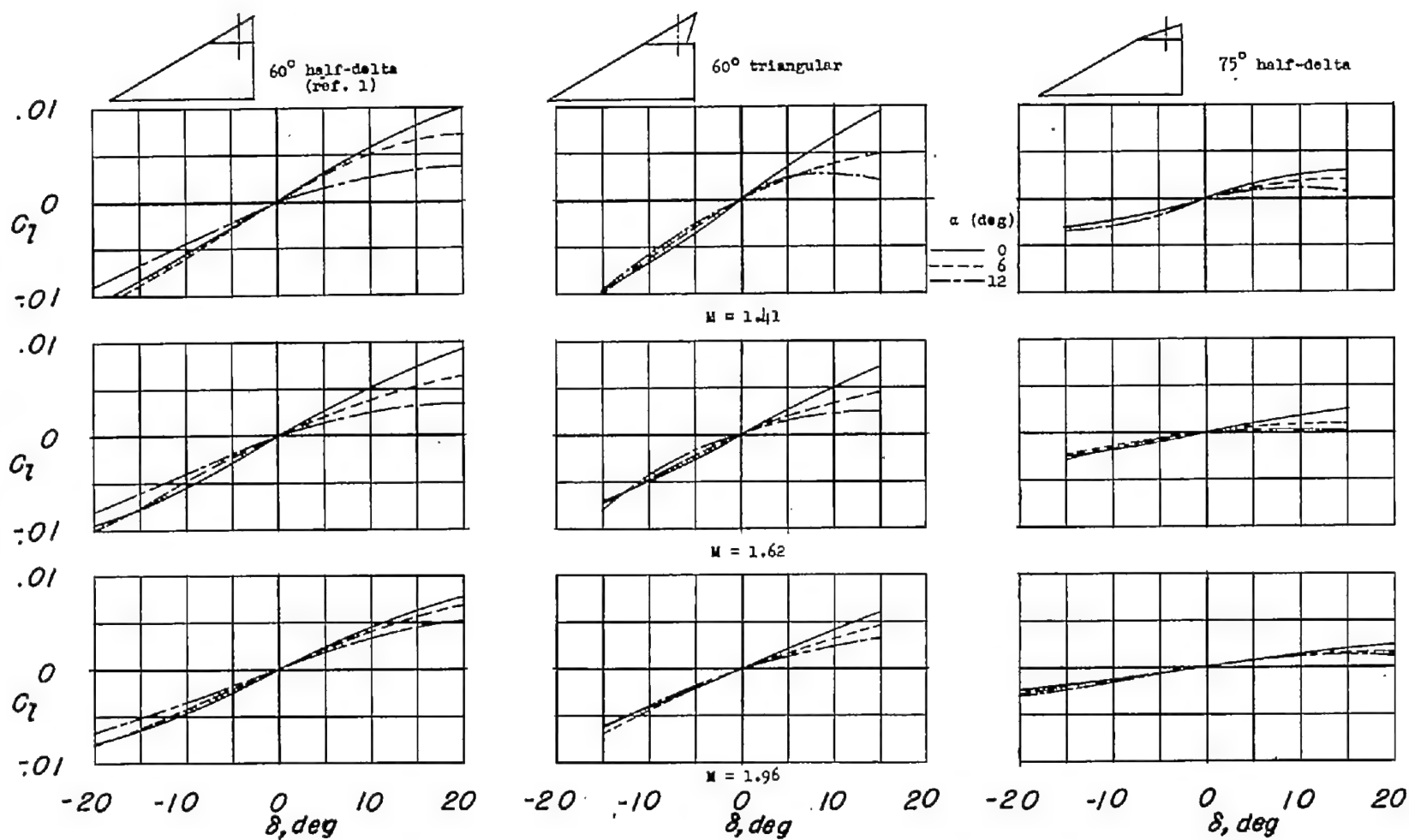


Figure 7.- Variation of rolling-moment coefficient with deflection for tip controls of three plan forms.  $R = 2.4 \times 10^6$ ,  $2.25 \times 10^6$ , and  $2.0 \times 10^6$ ;  $M = 1.41$ ,  $1.62$ , and  $1.96$ , respectively.

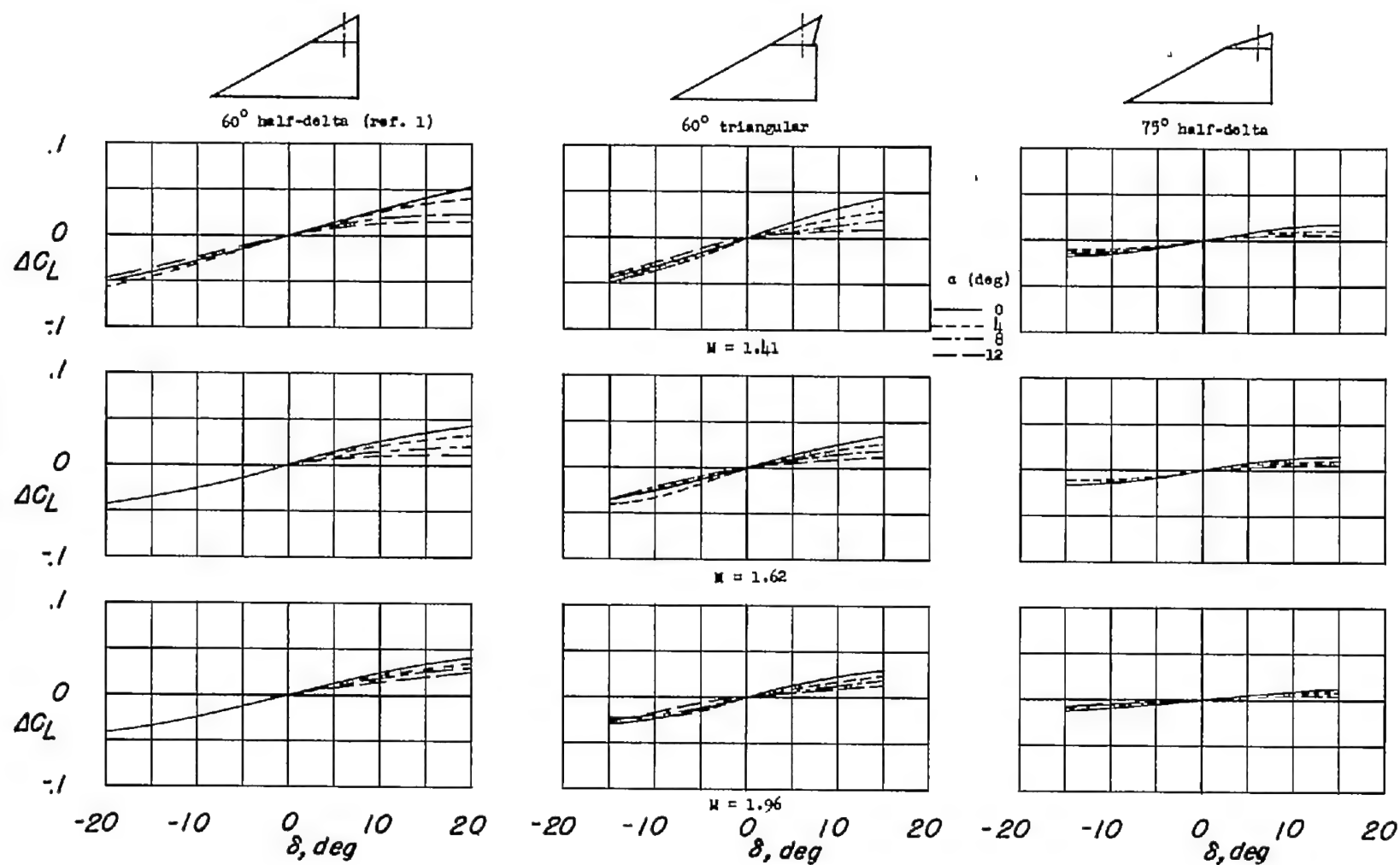


Figure 8.- Variation of the increments of lift coefficient with deflection for tip controls of three plan forms.  $R = 2.4 \times 10^6$ ,  $2.25 \times 10^6$ , and  $2.0 \times 10^6$ ;  $M = 1.41$ ,  $1.62$ , and  $1.96$ , respectively.

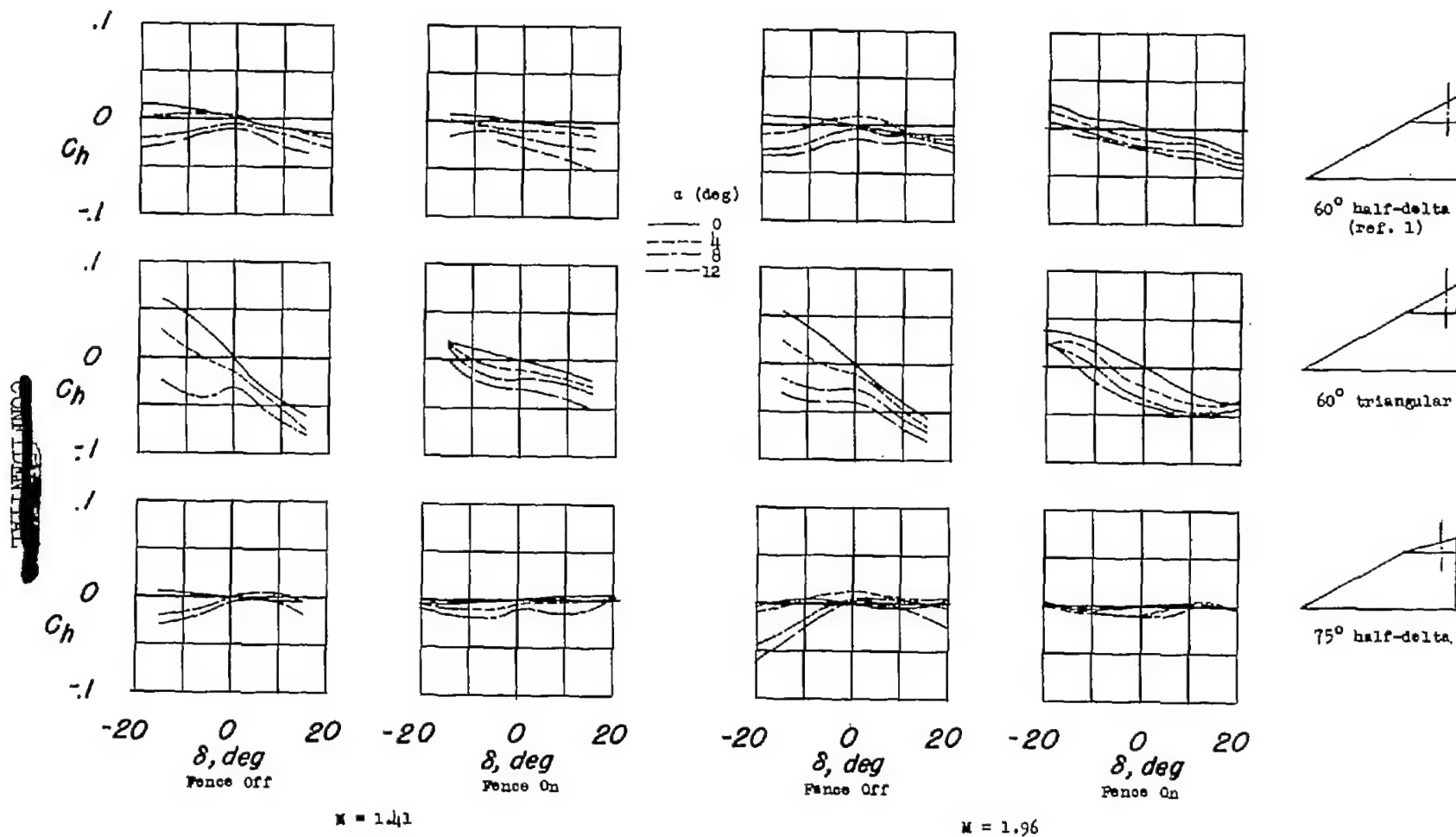


Figure 9.- Comparison of hinge-moment coefficients with and without fence for tip controls of three plan forms.  $R = 2.4 \times 10^6$  and  $2.0 \times 10^6$ ;  $M = 1.41$  and  $1.96$ , respectively.

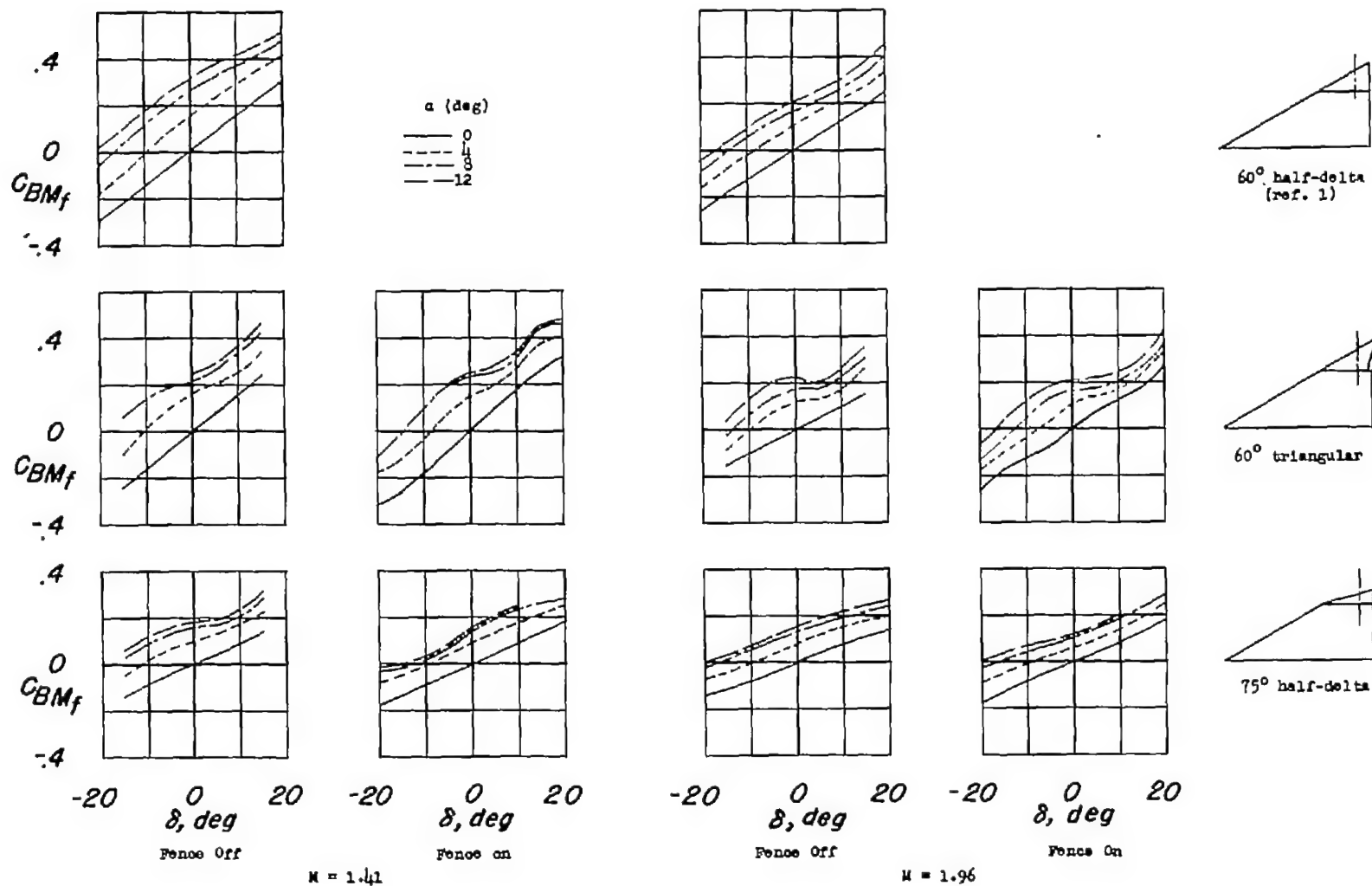


Figure 10.- Comparison of bending-moment coefficients with and without fence for tip controls of three plan forms.  $R = 2.4 \times 10^6$  and  $2.0 \times 10^6$ ;  $M = 1.41$  and  $1.96$ , respectively.

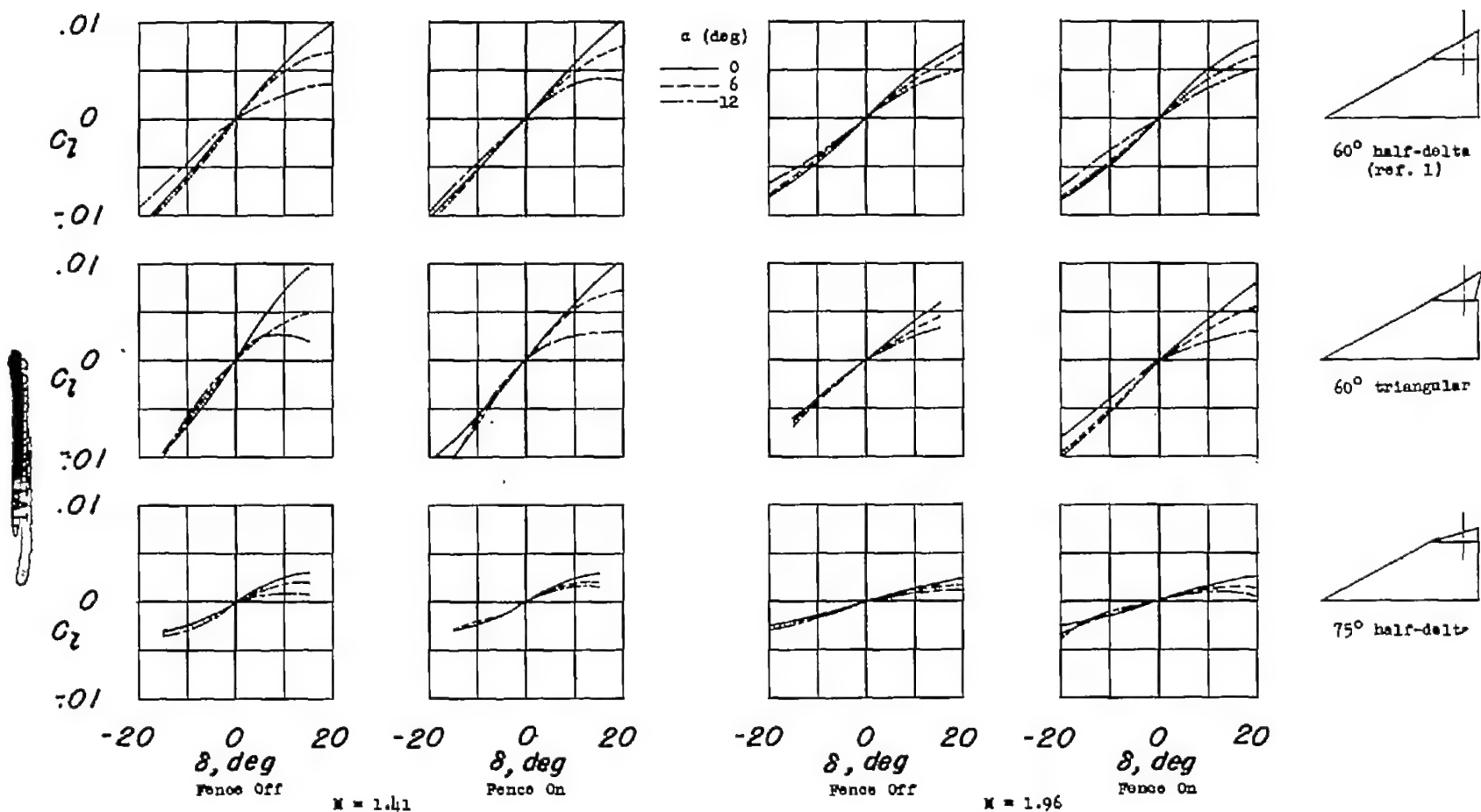


Figure 11.- Comparison of rolling-moment coefficients with and without fence for tip controls of three plan forms.  $R = 2.4 \times 10^6$  and  $2.0 \times 10^6$ ;  $M = 1.41$  and  $1.96$ , respectively.

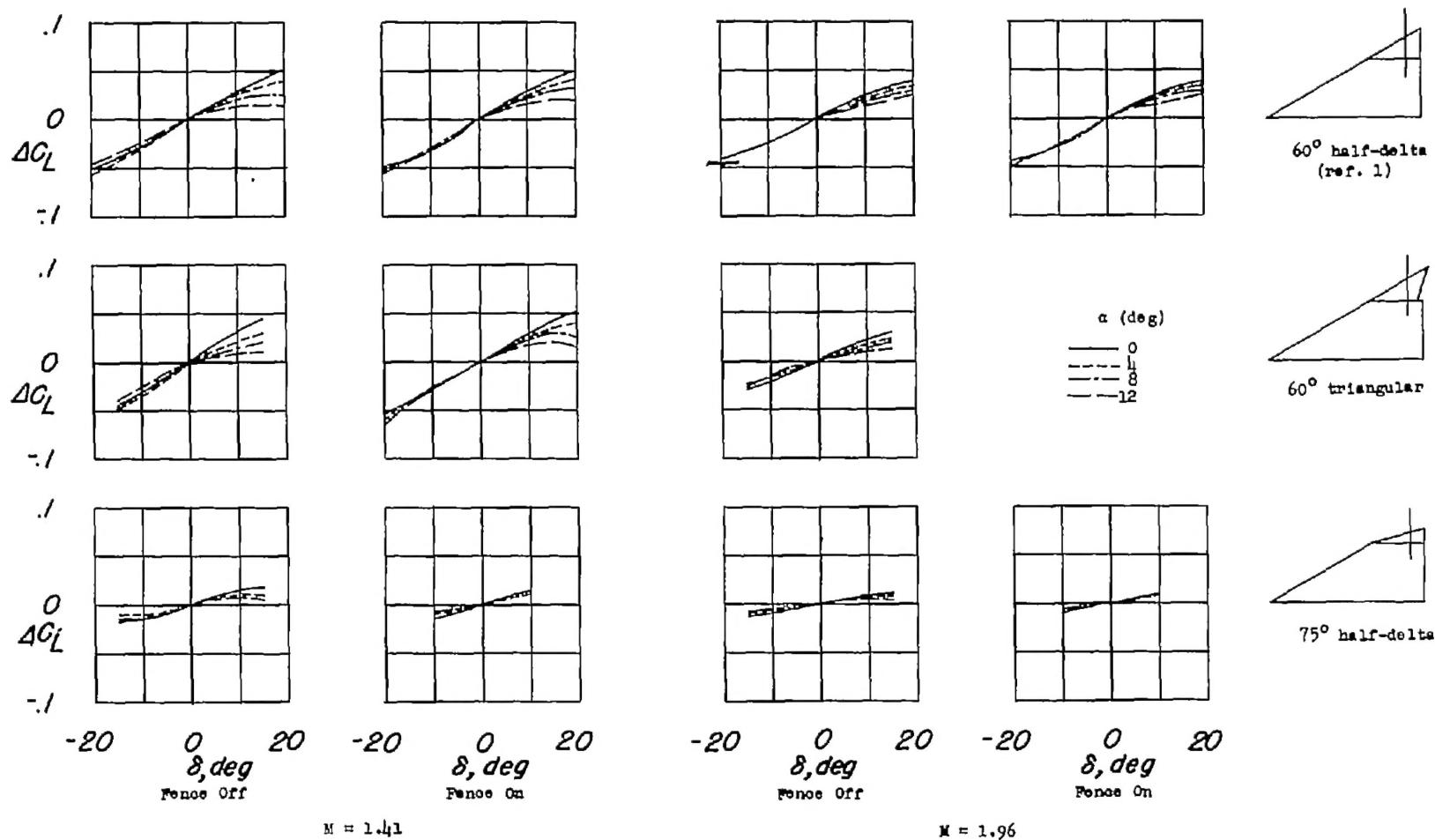


Figure 12.- Comparison of the increments of lift coefficients with and without fence for tip controls of three plan forms.  $R = 2.4 \times 10^6$  and  $2.0 \times 10^6$ ;  $M = 1.41$  and  $1.96$ , respectively.



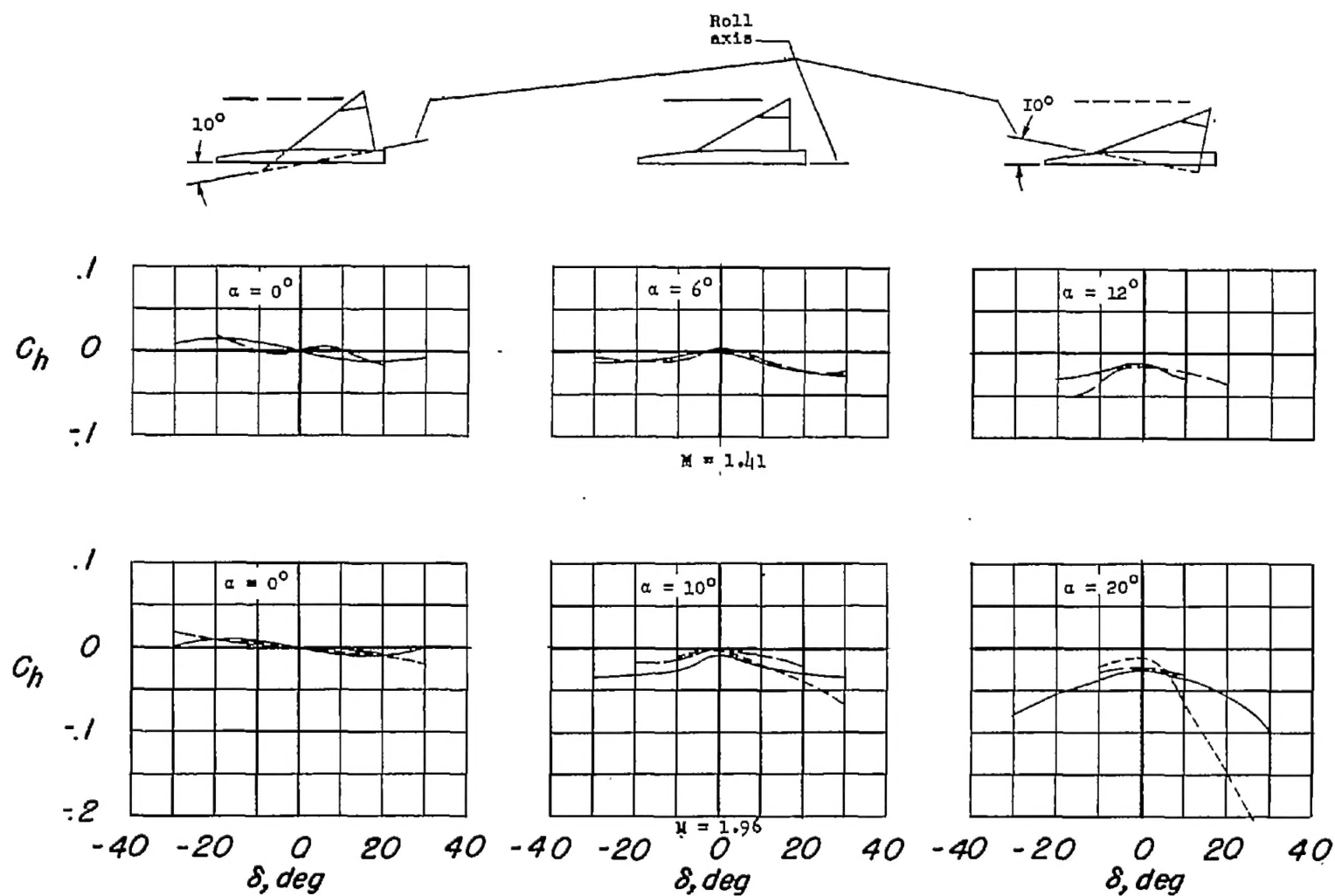


Figure 13.- Effects of wing skew on the variation of hinge-moment coefficient with deflection for a  $60^\circ$  half-delta control.  $R = 2.4 \times 10^6$  and  $2.0 \times 10^6$ ;  $M = 1.41$  and  $1.96$ , respectively.

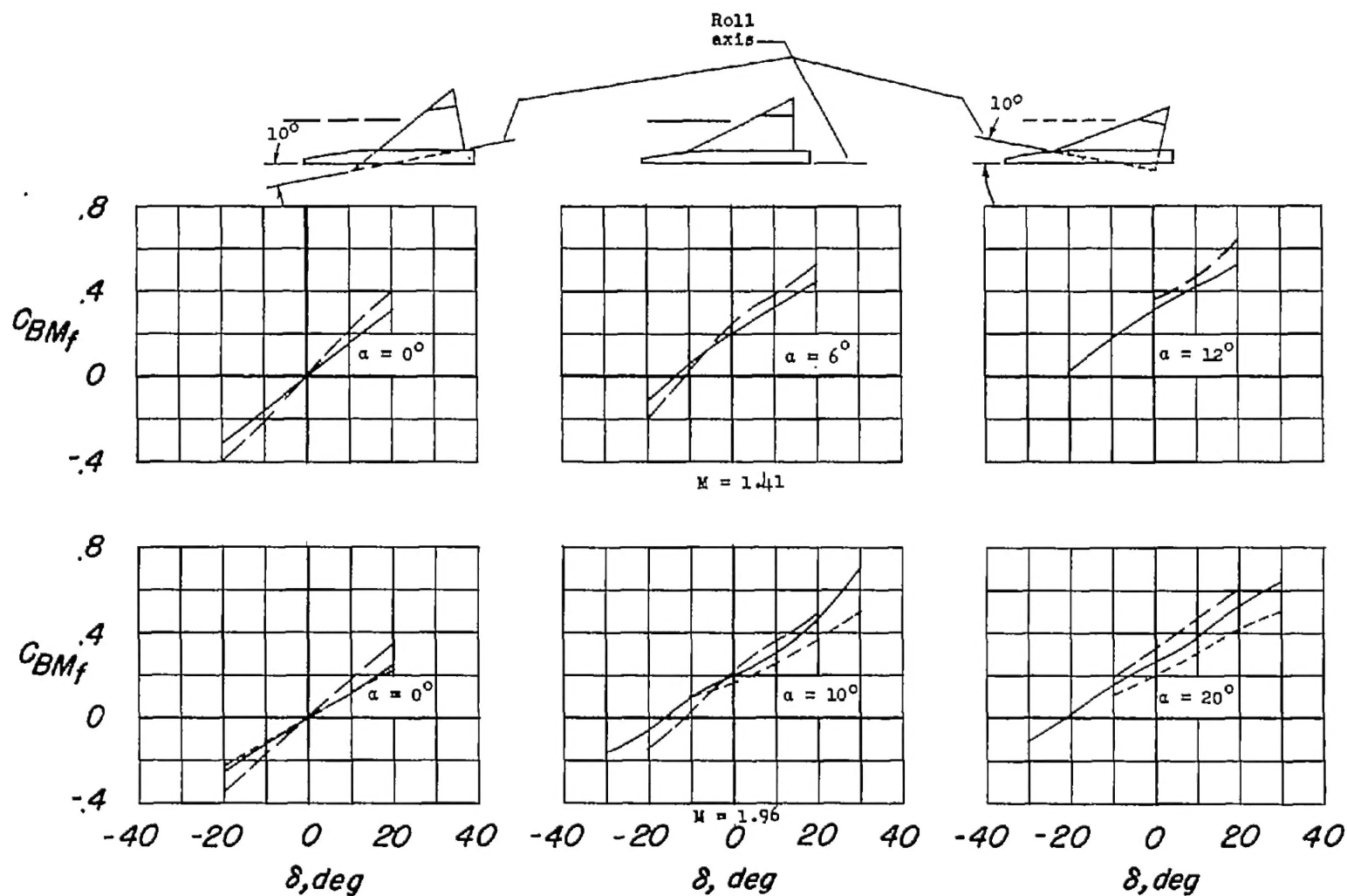


Figure 14.- Effects of wing skew on the variation of bending-moment coefficient with deflection for a  $60^\circ$  half-delta control.  $R = 2.4 \times 10^6$  and  $2.0 \times 10^6$ ;  $M = 1.41$  and  $1.96$ , respectively.

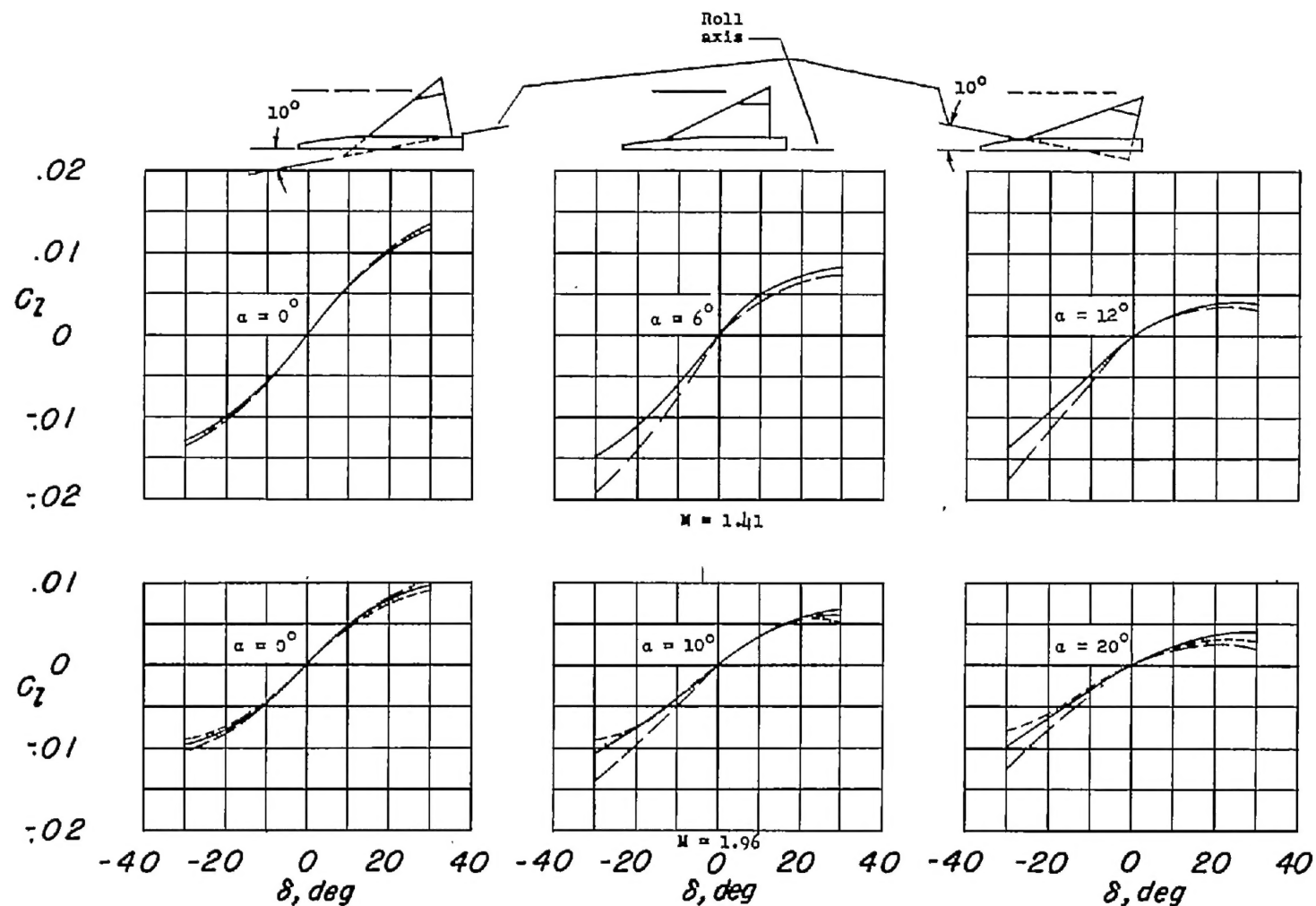


Figure 15.- Effects of wing skew on the variation of rolling-moment coefficient with deflection for a  $60^\circ$  half-delta control.  $R = 2.4 \times 10^6$  and  $2.0 \times 10^6$ ;  $M = 1.41$  and  $1.96$ , respectively.